

SPECIFICATION

TITLE

METHOD FOR COOLING COILS AND SHIM IRON

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention generally concerns the cooling of electrical coils. The present invention thereby in particular concerns a novel cooling method for better heat dissipation at gradient coils and shim systems of nuclear magnetic resonance tomography apparatuses.

10 Description of the Prior Art

Electrical coils generally possess a power or, respectively, stability limit that is defined by the limited dissipation of the heat due to ohmic loss heat. Such coils are used in magnetic resonance tomography (MRT), for example in the form of gradient coils and shim coils.

15 Gradient coils serve for the spatial coding inside an MRT apparatus ~~in that~~
by generating a three-dimensional orthogonal gradient field that is superimposed
on the static homogeneous basic magnetic field in the x-direction, y-direction and
z-direction. The x-coil and y-coil are typically ~~what are~~ a coil type known as
saddle coils that are rotated against with respect to one another by 90° with
20 regard to the z-axis. The z-coil represents a Maxwell coil.

An exact image reconstruction in MRT is only possible when, during the measurement, the gradient coils exhibit a sufficient temporal magnetic field stability ~~on the one hand~~ and the static basic magnetic field is sufficiently homogeneous ~~on the other hand~~.

25 Among other things, two techniques are known for homogenization of the basic field magnets:

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1. A further orthogonal coil system with current flowing through it is located within the orthogonal gradient system, with which ~~further orthogonal coil system~~ it is possible to homogenize the basic field magnet. These additional correction coils (also called shim coils) serve to compensate field inhomogeneities
5 of higher ~~order~~ orders and are designed in a very complicated manner in that they are interwoven with the gradient coils.

2. For further homogenization of the basic magnetic field, a suitable arrangement of ~~magnet~~ paramagnetic bodies (shim irons) that are integrated into the gradient coil is calculated with the aid of a field calculation program. The
10 curve of the magnetic field lines of the base field and of the gradient fields can be influenced ~~via~~ by the size and position of the shim irons. An advance measurement of the field distribution serves as a ~~specification~~ basis for the calculation. Another control measurement is conducted after the mounting. This process must be repeated multiple times before a satisfactory shim result is
15 achieved. The shim irons ~~are~~ typically are introduced into drawers axially in ~~what~~ are openings known as shim channels in the tube wall of the gradient system. In order to avoid or, ~~respectively~~, to minimize eddy currents in the shim irons, the respective shim iron blocks (~~made up~~ composed of playing card-sized shim plates) are stacked.

20 ~~While the~~ The technique under point 1 ~~represents an~~ is known as active shimming shim, the technique under point 2 is ~~designated~~ known as a passive shimming technique. The combination of both techniques ~~represents what~~ is known as a shim system.

25 ~~It is object~~ The purpose of the gradient coil current supply and shim coil current supply ~~is~~ to generate current pulses of precise amplitude and at precise times, corresponding to the measurement sequence used. The required currents are approximately 250 amperes, the current rise rate is in the range of 250 kA/s.

Under such conditions a ~~great deal~~ large amount of heat arises in the gradient coils and in the shim coils due to electrical power loss on the order of

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approximately 20 kW, which heat must be actively dissipated in order to prevent that the electromagnetic behavior of the gradient and shim system (and therewith the imaging itself) is from being impaired.

A heating of the shim irons (~~on the one hand due in part to ohmic losses of~~ 5 ~~eddy currents that cannot be avoided, on the other hand due in part to heat transfer of the gradient and shim coil heat via the sealing material~~) cannot be avoided and would significantly impair the shimming if the shim irons were not also cooled. However, the heating of the shim irons is smaller by orders of magnitude (approximately 5 W) than that of the gradient coils and shim coils, 10 which is why an elaborate active cooling of the individual shim irons is not absolutely necessary.

According to the prior art, the cooling of convention electrical coils ~~but also as well as~~ 15 ~~the cooling of gradient coils, shim coils and shim irons in nuclear magnetic resonance tomography ensues either via by air surface cooling (air blown past) or via by water cooling. The execution of an active Active~~ water cooling has previously conventionally represented the most efficient cooling. However, the The heat is hereby typically transferred from the conductors to be cooled into heat-dissipating flowing water via more or less poorly-conductive plastic layers. The heat resulting resistance thereby caused to heat flow limits the 20 maximal capacity of the water cooling.

SUMMARY OF THE INVENTION

~~It is therefore the An object of the present invention is to achieve provide~~ a cooling system with a much more efficient cooling capability in order to cool electrical coils and heat sources with low technical expenditure, in particular in 25 magnetic resonance tomography.

~~This object according to the present invention is achieved via the features of the independent claims. The dependent claims thus develop the central ideas of the invention in a particularly advantageous manner.~~

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According to The above object is achieved in accordance with the invention by an electrical coil with a cooling system is claimed, whereby wherein the cooling system comprises includes a heat dissipation device with a fluid and a tempered reservoir of containing this fluid, and whereby wherein the coil is coupled to the 5 tempered reservoir by means of the fluid, and the reservoir is temperature-regulated such so that the temperature as well as the pressure of the fluid is kept in the immediate proximity of the critical point of the fluid.

In a first embodiment of the invention, the coupling ensues via a tube that conducts heat well, which tube contains the fluid and is situated in thermal contact 10 with the coil conductor in that it passes through the electrical coil.

In a second embodiment of the invention, the coupling exists ensues via the conductor of the electrical coil itself, in that this is fashioned tube-like and contains the fluid.

In a third embodiment, the coupling ensues via a heat-insulating tube inside 15 which the coil conductor is coaxially directed and which simultaneously contains the fluid.

The critical temperature of the fluid advantageously corresponds to approximately room temperature.

According to the invention, carbon dioxide or C_2F_6 is suitable for use as the 20 fluid inasmuch offers itself [sic].

In order to generate an achieve optimal cooling, the temperature and pressure of the fluid in the reservoir are kept in immediate proximity of the critical point via by a heat exchanger.

In a particular another embodiment of the invention, the electrical coil 25 represents is a gradient coil for a nuclear magnetic resonance tomography apparatus with an electrical coil with a cooling system according to any of the preceding claims [sic], whereby the as described above. The gradient coil is can be a transversal transverse gradient coil and/or an axial gradient coil.

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In a further embodiment of the invention, the electrical coil ~~represents is~~ a shim coil for a nuclear magnetic resonance tomography apparatus with ~~an electrical coil and a cooling system as described above according to any of the preceding claims [sic]~~.

5 According to The above object also is achieved in accordance with the invention[[,]] by a nuclear magnetic resonance tomography apparatus ~~is also claimed with~~ shim irons and a cooling system, whereby wherein the cooling system ~~comprises~~ has a heat dissipation device with a fluid and a tempered reservoir ~~of~~ containing this fluid, and whereby wherein the shim irons ~~is [sic]~~ are 10 coupled to the tempered reservoir by ~~means of a~~ the fluid and the reservoir is temperature-regulated ~~such so~~ that the temperature as well as the pressure of the fluid is kept in immediate proximity of the critical point of the fluid.

15 In an ~~advantageous~~ embodiment of the invention, the shim irons are disposed in shim iron channels that are thermally coupled to a tube system containing the fluid.

Here it is also ~~advantageous when the~~ The critical temperature of the fluid preferably approximately corresponds approximately to room temperature.

It is ~~inasmuch~~ advantageous to use carbon dioxide or C_2F_6 as the fluid.

According to the invention, the temperature and pressure of the fluid in the 20 reservoir ~~is [sic]~~ are kept in the immediate proximity of the critical point ~~via by~~ a heat exchanger.

DESCRIPTION OF THE DRAWINGS

Further advantages, features and details of the present invention are now explained in detail using exemplary embodiments referencing the accompanying 25 drawings.

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Fig. 1 shows in perspective the gradient shim system of a MRT apparatus with a coupling of two shim channels to a fluid reservoir in accordance with the invention.

Fig. 2 shows a possible an embodiment wherein coupling of an electrical 5 coil via the conductor itself.

Fig. 3 shows a possible an embodiment wherein coupling of an electrical coil via a coaxially-directed conductor in a fluid-filled insulator.

Fig. 4 shows a possible an embodiment wherein coupling of an electrical coil ensues via fluid-filled thermal conductor that is in thermal contact with the 10 electrical conductor of the coil at suitable points.

Fig. 5 shows the anomaly of the heat conductor coefficients of CO₂ in the proximity of the critical point.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

As already shown described above, electrical coils (such as, for example, 15 sealed gradient coils or shim coils in MRT apparatuses) are presently air- or water-cooled, which leads to a distinct limitation of the heat dissipation capacity due to the poor heat conductivity of the sealing material. The present invention represents a significant improvement of over such conventional cooling systems. For heat transfer, it is proposed to utilize the nearly unlimited large heat 20 conductivity of fluids in the range of their critical point is utilized.

The anomaly of the heat conductivity coefficient coefficients λ of fluids a fluid in the proximity of the critical point has been long known and is, for example, briefly described in the book "The properties of gases & liquids, Reid, Prausnitz, Poling, McGraw-Hill Book Company, 4th edition, ISBN 0-07-051799-1" on the 25 pages 518 through 520.

The heat conductivity λ of carbon dioxide (CO₂) is graphically represented in Fig. 5 dependent on the density at different temperatures (Fig. 5 was taken from

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the mentioned aforementioned literature passage). Shown are four curves of λ (measured in W/mK) in the range of the critical density ($p_c = 0.468$ g/cm³) at temperatures of 75, 40, 34 and 32 °C. The graphic graph shows a distinct, significant rise of λ in a relatively narrow range of the critical density (± 0.1 g/cm³)

5 the more that the temperature approaches the critical temperature ($T_c = 31$ °C). The λ of CO₂ at 32°C is thus already six times (0.3 W/mK) the value as at 75 °C (0.05 W/mK). Ultimately, at 31°C a nearly infinite value is theoretically expected (not shown in Fig. 5).

A clear explanation of this phenomenon is not provided. The conjecture is
10 merely expressed that microscopic molecular phase or, ~~respectively~~, order transitions could be responsible or, ~~respectively~~, microscopic flow effects due to molecular cluster movements.

A technical application of this effect was described for the first time in "German Jet Engine and Gas Turbine Development 1930-1945, Anthony L. Key,
15 Airlife, England" on the pages 214/215. In the framework of examinations regarding cooling methods given for gas turbine blades, Prof. Ernst Schmidt began in 1938 with studies of the heat conductivity of fluids in the range of the critical point. In order to demonstrate the theoretically infinite heat conductivity at the critical point, ~~he filled a steel tube~~ was filled to one-third with liquid ammonia
20 (NH₃). With practically all gases the density in the fluid state corresponds to approximately three times the density of the critical state. The cited ammonia filling to a third ~~therewith~~ also simultaneously leads to the critical pressure at the critical temperature. After a heating to 20°C, the tube ~~possessed~~ exhibited a heat conductivity like that of pure copper. After further temperature increase to the
25 critical temperature ($T_c = 132$ °C) – it is reported – the heat conductivity of the tube now exceeded that of copper by 20 times.

For cooling of gas turbine blades, the described effect was translated to water, ~~in that~~ by water vapor with critical temperature (374°C) was ~~pushed~~ being forced through turbine blades at a critical pressure of 76 bar.

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According to the present invention, the described effect ~~should be~~ is utilized to keep electrical coils (as ~~they~~ are, for example, used in MRT apparatuses as gradient coils and shim coils) at operating temperature. According to the invention, for this purpose the portion of the conductor piece to be cooled is

5 thermally coupled to a fluid reservoir via a heat sink (for example a cooling tube). The fluid system is filled with a fluid at approximately critical temperature and critical pressure. This pressure and this temperature ~~is~~ are maintained or, respectively, regulated ~~via~~ by a heat exchanger or, respectively, a pressure regulator.

10 The segment conductor portion to be cooled thus ~~stands~~ is in direct contact with the fluid reservoir in this manner via extremely good heat conduction. The transport of a carrier medium for heat dissipation to the point to be cooled (as ~~was~~ previously ~~given~~ necessary for active water cooling) is no longer necessary. For this reason no boundary layer effects (Prandtl boundary layer) that distinctly
15 significantly increase the heat transfer resistance exist in the inventive fluid system.

The viscosity of the fluid as a static medium is ~~also extraneous~~ not relevant in the inventive cooling system. The heat capacity of the fluid is only important insofar as it concerns the rapidity of the heat dissipation of the reservoir (and
20 therewith the regulation inertia of the fluid system. In contrast to heat pipes, gravity (~~gravitation~~) has no influence; the heat conduction ensues similarly in the fluid in every spatial direction.

C₂F₆ ~~lends itself~~ is suitable as a filling gas for the operation at room temperature (approximately 293 K, 20°C), the critical pressure of which is a
25 controllable 30 bar and ~~whose~~ the critical temperature of 292 K (19°C) lies only a little below the operating temperature.

CO₂, with a critical pressure of 72 bar and a critical temperature of 301 K (minimally above the operating temperature), would also be suitable ~~possible~~. The latter has the advantage that a slight heating even further improves the

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already high thermal conductivity due to approach of approaching the critical point and therewith stabilizes the temperature of the conductor.

According to the invention, various types of thermal coupling of the element (coil conductor or shim iron) to be cooled are possible.

5 In a first exemplary embodiment according to Fig. 2, the coil conductor is fashioned as a tube 1 in which the stated aforementioned fluid 2 is located.

In a second exemplary embodiment according to Fig. 3, the conductor 3 is surrounded by a fluid-filled hollow tube 4 whose tube wall is electrically insulating and poorly thermally conductive, such that the heat is conducted along the tube 10 inside 4; surrounding carrier structures are, however, not heated. The conductor 3 can be held (for example as in a coaxial cable) with support ribs 5 in the hollow tube 4.

In both exemplary embodiments the tube inside 2 is connected with the cooled fluid reservoir.

15 In a third inventive embodiment according to Fig. 4, the electrical coil 9 to be cooled is pervaded with a separate fluid-filled tube 7 which has thermal contact with the coil conductor 9 at a plurality number of points 8 and is connected at least at one end with the cooled fluid reservoir 6.

As already mentioned above in the specification preamble, it is normally 20 also necessary to cool the shim irons 10 in order to ensure or, respectively, maintain the homogeneity of the basic magnetic field. Although the heating of the shim irons 10 is much lower than that of the gradient or shim coil conductor, a heat dissipation is necessary, whereby here for which the described effect can also be utilized according to the invention.

25 The shim irons are typically are arranged in drawer-like insertions 11, whereby the. The number of the shim plates 12 in the different shim irons (also called shim stacks) can by all means be different. For example, Fig. 1 shows an insertion 11 with three shim irons (shim stacks) 10, whereby the front stack

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comprises having five shim plates 12, the middle stack comprises having three shim plates 12 and the rear stack comprises having two shim plates 12. An insertion 11 with sixteen to eighteen shim iron stacks is normally respectively located in a shim channel 13, with sixteen shim channels in total that are radially, 5 uniformly distributed in the gradient coil body 14, preceding and run axially. The insertions 11 are axially inserted on at the front side.

A ~~cooling~~ Cooling of the shim irons 10 using the effect described above ensues according to the invention via a coupling of all shim channels 13 (in which are respectively located the drawer-like insertions 11) to a tempered fluid reservoir 10 6. The coupling ensues via (thermo) hoses conduits 15 that are flanged on at the front side thereof at the corresponding shim channels 13. Two such hoses conduits 15 are shown in Fig. 1. Each shim channel 13 is filled with the fluid 2 which is tempered ~~via the hoses in~~ by communicating the conduits 15 with the reservoir 6 at critical temperature. The heat of the shim irons 10 is directly 15 dissipated via the fluid reservoir 6 in this manner.

A less elaborate cooling of the shim irons 10 is to couple the hoses conduits 15 with a passive heat sink, for example with an outer covering hull of the basic field magnet, and to forego ~~a~~ the fluid reservoir 6 ~~to be~~ tempered. Such a design of the shim iron cooling is, however, only is efficient only when a certain 20 heat capacity of the shim irons 10 is not exceeded.

Although modifications and changes may be suggested by those skilled in the art, it is the invention of the inventor to embody within the patent warranted heron all changes and modifications as reasonably and properly come within the scope of his contribution to the art.